## - NA1001 -

## 1.0kW FM POWER AMPLIFIER

## USER AND MAINTENANCE MANUAL



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## NA 1001 <br> 1.0kW FM POWER AMPLIFIER

TheNA1001 is a highly integrated broadband solid-stateMos-Fet FM amplifier of 1000W rated power, fitted in a 4 unit 19 " rack, which dont require any specific calibration to operate in the $87.5 \div$ 108 MHz frequency range.

Its compact size, high efficiency, wide ACrange acceptance, low maintenance requirements and broadband construction, make this amplifierideal in medium powerrepeaters, in unattended posts, in $\mathrm{N}+1$ systems and as a reserve.

Its sturdy, modular mechanical and electrical construction guarantees a high MTBF and an easy maintenance. The modules are easily identifiable and inspectable with few interconnections with each other, throughmulti-pole connectors.

The nominal RF output power is obtained over the full FM range with a mere 12 W drive and is particularly stable against time, temperature and frequency variations being ALC regulated, with a front panel adjustment. The output power may be varied from a minimum level to the nominal level and the frequency varied over the full FM range, without retouching the drive power or any other adjustment than the ALC control.

The output stage has a reverse intermodulation figure, which is lower than standard bipolar construction, due to the all Mos-Fet design and approaches that of tube equipment.

A simple metering and alarm section completes the amplifier, permitting an easy check of the functions withfew, unambiguous readings. Powerreadings and control are externally availableon a remote I/O port, for an external controller.

The whole assembly is designed in accordance with the CCIR, FCC and tighter international norms and conforms to the recent, strict requirements for EMI susceptance and emission.

## C <br> This equipment complies in particular to ETSI EN300.384 and EN 300.447 Broadcast and EMI/EMC standards, EN60065 and EN60215 safety standards and FCC parts 73 \& 74.

### 2.1 FRONT PANEL COMMANDS AND SIGNALLING



The front control panel carries the power on switch, the control meter, some alarm warningLED's and a RF monitor connector. On the bottom, a panel grid allows for ventilation.

At the RF monitor output, (BNC type), a sample of the output power is available which is attenuated 54 dB typically (i.e. $+6 \mathrm{dBm} @ 1.0 \mathrm{~kW}$ output). Even if this output is fairly flat vs.frequency, one should not use this for accurate harmonic analysis.

The switchable meter permits the reading of the most important operating parameters, i.e. the forward and reflected power( $1250 \mathrm{Wf.s}$.) and the regulated and unregulated power supply voltage (300Vdcf.s.).

The 2LED'slight only in case of failure. The meaning of these LED is summarised on the following table:

### 2.2 THE REAR PANEL AND THE CONNECTIONS

| LED | MEANING |
| :--- | :--- |
| VSWR | High RF output reflected power $(>80-100 \mathrm{~W})$ |
| TEMPERATURE | High internal temperature, probably due to high environment temperature <br> or failure of the ventilation system. |

Table 1: warningLEDmeaning

The rear panel allocates the RF power and the I/O ports in addition to the mains power cord and

fuse, the grounding screw and an auxiliary AC socket on some models. The power cord is not removable. If it is required a longer cable than that provided in the factory (roughly 2 meters long), a suitable $3 \times 1.5 \mathrm{~mm}$ sq. power cord may easily replace the original one. The fuse has a differentrating for 115 or 230 Vac operation: be sure to adopt the right type for your power network.

The Antennaoutput is brought out on a $7 / 8$ " connector, while the input connector is a "N" type. A remote I/O port is available on aSUBD 25 poles, female connector.

The exhaust air output opening must not be obstructed during operation: wide spacing must be provided duringinstallation topermita sustained ventilationair flow.Inserting the equipment in aclosed rack without a suitable external air extraction system will damage the equipment and void the warranty.

An auxiliary IEC-320 female type power outlet is provided, which is powered only when the amplifier is on, to supply the exciter. No fuses other than the general fuses (16A) are inserted on this line. Limit the power absorption from this outlet to low levels, i.e. 100W/1A max.


Setting the AC voltage for $\mathbf{1 1 5}$ or $\mathbf{2 3 0 V}$ operation requires to gain access to the inner of the equipment, removing the top cover. Be sure to remove the power cord from power to avoid direct exposure to hazardous mains voltage, which are always present on the fuses and the input board, even with power on switch in the off position.

### 2.3 TECHNICAL SPECIFICATIONS

@ 1 kW RF output if not otherwise specified

- Frequency range:
$87.5 \div 108 \mathrm{MHz}$
- RF input power

12 W nom., $15 \mathrm{~W} \max$

- RF output power
$1000 \mathrm{~W} \pm 0.5 \mathrm{~dB}$
- RF input/output impedance:
$50 \Omega$
- RF input connector:

N

- RFoutputconnector: 7/8"
- RF monitor connector:

BNC

- Harmonic and spurious emissions: <-70 dBc
- RF monitor attenuation:

54 dB , typ.

- Max total current handling capability on the auxiliary socket:

1A @ 230 Vac, 100Wmax, not fused

- Mains supply requirements: $\quad 190 \div 250 \mathrm{Vac} 50 / 60 \mathrm{~Hz}<1900 \mathrm{~W}(2500 \mathrm{VA})$
- Operating temperature range: $\quad 0 \div+35^{\circ} \mathrm{C}$ recommended, $-10 \div+45^{\circ} \mathrm{C}$ max
- Dimensions, not including thehandles: $19^{\prime \prime} \times 7$ " x 21 " $(483 \times 177 \times 535 \mathrm{~mm})$ See drawings
- Weight: approx. 66 Lbs ( 30 kg .)


### 2.4 I/O REMOTE CONTROL SPECIFICATIONS

A remote I/ODB25 female connector, located on the rear panel, makes available 3 analog lines to permit remote control and surveillance of the equipment as detailed:

| Pin | Line | Range/use |
| :--- | :--- | :--- |
| $1,3,21$ | ground | common |
| 9 | Reflected Power | $0 \div 5 \mathrm{~V}$ vs. $0 \div 1300 \mathrm{Wout} \mathrm{Zo}=10 \mathrm{k} \Omega \quad(4 \mathrm{~V}$ typ. @ 1000W) |
| 10 | Forward Power | $0 \div 5 \mathrm{~V}$ vs. $0 \div 1300 \mathrm{Wout} \mathrm{Zo}=10 \mathrm{k} \Omega \quad(4 \mathrm{~V}$ typ. @ 1000W) |
| 13 | Power control | External RF output control. $0-5 \mathrm{~V}$ to full scale, low impedance |

The remote I/O signal and control DB25 female connector, on the rear panel


### 3.1 FOREWORD TO INSTALLATION

Although in most cases no special instruments are required, have skilled personnel install the apparatus. To make best use of the apparatus's capabilities and prevent damage to the unit, comply with the recommendations throughout this manual.

When in doubt, or if any technical problems should arise during the installation procedure, NICOM strongly recommend the apparatus not be tampered with in any way by unskilled personnel and will be glad to supply qualified after-sale service.

As a rule, the user should not have access to the inside of the apparatus for normal installation and use. Tampering with the factory settings makes the guarantee null and void and might also affect apparatus' performance, causing costly damage.


NO ADJUSTMENT OR INTERNAL PRESETTING IS REQUIRED FOR NORMAL OPERATIONS. THE APPARATUS SHALL BE PROPERLY GROUNDED AND BE OPERATED WITH ALLTHE COVERS CLOSED TOPREVENT ELECTRICALHAZARDS IN OPERATION AND FULLY COMPLY WITH CE EMI AND SAFETY REQUIREMENTS.

NEVER TOUCH THE INSIDE OF THE APPARATUS WITHOUT FIRST DISCONNECTING IT FROM THE POWER. DANGEROUS AC, DC AND RADIO-FREQUENCY VOLTAGES ARE PRESENTINSIDE AND BECOME ACCESSIBLE WHEN THECOVERS AREREMOVED.

### 3.2 INSTALLATION

Install apparatus in adry, sheltered but well-ventilated room away from dust, moisture, insects and vermin(mice).

Place apparatus as close as possible to the antenna to prevent excessive power loss in the cables. If this is not feasible, use antenna cables of suitable cross-section.

Room size shall be such that the apparatus can be placed in an upright position and that technical personnel caneasily carry outroutine orextraordinary maintenance. The minimumrecommendedsize is 2.5 mx 2 m , and 2.2 mhigh when there is no other broadcasting or support equipment nearby.

The room must be ventilated to ensure that the inside temperature never exceeds $35^{\circ} \mathrm{C}$. Even if $45^{\circ} \mathrm{C}$ is the max. allowed temperature: it is anyway suggested not to approach to this limit.

This condition cannot generally be met when the exhaust cooling air is not pushed outside and is fed back into the room. This is even truer if more than one apparatus is installed in the same location. An efficient ventilation system is thus required in the room. Air exchange in the room shall have a minimum flow-rate of 500 metres cubed per hour or more.

If the apparatus is fitted in a rack system, the back door of the rack cannot usually be fixed in place. If a completely closed assembly is needed, a suitable ventilation extraction unit must equip the system. To aid air ducting, an optional flange may be retrofitted on the ventilation outlet to which aduct can be attached to convey hot airoutside. In this caseremember that the NA1001 internalfans are low-pressure units: some sort of external air extraction bloweris thanimperative on the exhaust airduct.

Vents in the walls and any other openings shall be fitted with a metal grating to keep rodents out, and with a dust filter. Make absolutely certain that no water can seep through the vents or the air exhaust duct or antenna-cable grommet, and that the floor cannot be flooded during heavy rainfall. If notimpedited by proper airfiltering, insects in somelocation may be conveyed in the internal heatsink, accumulating on it and finally obstructing it, causing theovertemperature alarm to be triggered.

Even moisture and/ordust, whencontained in the airor intheroominexcessive quantity, may cause condensation build-up in the amplifier. When the system is periodically switched on and off, this can trigger destructive electric arcs and short circuits and thus cause damage that is not covered by the warranty.

### 3.3 WIRING INTO THE MAINS

The NA1001 is powered by a single-phase line. Power capacity must be at least 3 kVA and the
nominal voltage is 230 Vac . In some countries, where 115 Vac is the norm, this voltage mustbe internally set in the factory or by skilled people before installation.

While the power supply regulator accepts a wide input voltage ( $190 \div 250 \mathrm{Vac}$ ), operation near the lower input voltage on high impedance lines must be avoided: if the line drops more than 10 volt at full load, the low line sense circuitry may trigger an oscillating turn-on/turn-off cycle, which is very dangerous. In this case adopt an external line stabilizer.

The nominal power inputrange $(190 \div 250 \mathrm{Vac})$ is achieved when the primary side of the main transformer is wired to the 230 V tap. Two other taps, the first one slightly lower $(220 \mathrm{~V})$, the second higher $(240 \mathrm{~V})$, are available to adjust the input voltage range of $\pm 10 \mathrm{~V}$. In countries were a stable 240 V is the norm, it is important to set this tap on the transformer. In this case the allowed voltage range window must be shifted higher to avoid a nuisance trip atoccasional higher power voltage. See proper section in the service section of this manual.

Toensure proper operation and comply with the safety regulations, efficient grounding is required. Use the yellow/green lead in the powercable. The cable's neutrallead is blue.Never connect the earth to the mains' neutrallead.

The cable connecting the NA1001 mains input terminal block to the external board should consist of leads of adequate cross-section. Recommended values are 1.5 to 2.5 mm squared.

Do never switch the apparatus on without antenna connection, even when noRF drive is on.

### 3.4 ANTENNA CONNECTION

A 7/8" output connector is fitted at the back of the amplifier module. It is very important to check that the antenna, the connecting cables and the connectors are suitable for 1.0 kW .

The antenna coupler too, should be capable of adequate power; its input connector shall be 7/16" or $7 / 8$ " or larger.

The cable connecting the amplifier and antenna will generally be of the corrugated, spongy-dielectric type, such as a $1 / 2^{\prime \prime}$ or $7 / 8^{\prime \prime}$ celflex or flexwell. Smaller cables as RG214, cannot be used.

The antenna shall be earthen via a copper braid of adequate cross-section to prevent lightning reaching the amplifier via the antenna cable.

### 3.5 LF CONNECTION

To maximally avoid earth loops, wire the modulation signal line directly on the exciter, with high quality shielded and preferably balanced cable. Earth the shield only on the exciter LF input

If balanced lines are not feasible, use the highest available level: the suggestedNT30 exciters may easily accommodate signals at +6 or +10 dBm .

### 3.6 OTHER RECOMMENDATIONS

The ambient temperature shall range between $23^{\circ} \mathrm{F}\left(-5^{\circ} \mathrm{C}\right)$ and $86^{\circ} \mathrm{F}\left(+30^{\circ} \mathrm{C}\right)$.
It is advisable to hang a min.-max thermometer on the wall to display any variation.
Air conditioning at $20 \div 25^{\circ} \mathrm{C}$ would obviously be the best solution, but installation and operating costs are generally excessive. Thermal isolation and efficient ventilation with a thermostat-controlled blower are generally the most advantageous solution.

Power fluctuation andelectric discharges due to the weather or nearby industrial machinery may cause significant trouble, especially in mountain areas and in places close to industrial areas. In such cases, it is advisable if not indispensable, to install a protector, and insulating transformer or possibly an electromechanical power voltage regulator. NICOMcan provide all these accessories on request.

Since the total cost of the plant, inclusive of broadcasting equipment, antenna system and installation, is rather high, a certain percentage of the budget should be estimated for buying and installing suitable protection and conditioning facilities as described above.

Depending on location, the share of total cost should be around $20 \div 30 \%$; with this expenditure, however, the machinery will operate under optimum conditions, its useful lifespan will increase and, above all, the incidence of accidental breakdowns due to ambient or power trouble will be reduced.


# OPERATION WITHOUT THE ANTENNA OR WITH A FAULTY ANTENNA CONNECTION MAY CAUSE DEGRADATION AND POSSIBLE DESTRUCTION OF THE FINAL STAGE. THIS FAILURE ISNOT COVERED BY THE GUARANTEE. 

AVOID THE USE OFTOOPOWERFULEXCITER. AN INPUTPOWER HIGHER THAN 20W MAY PERMANENTLY DAMAGE THE RF TRANSISTOR CAUSING COSTLY DAMAGE, WHICH IS NOT COVERED BY THE WARRANTY. A STABLE AND PROPERLY REGULATED 20 $\div 25 \mathrm{~W}$ EXCITER, LIKE NICOM'S NT30 IS THE BEST CHOICE.

NA1001 drivenby atypical NICOM exciter generates a very clean RF output. Nevertheless if any strongRFsignal, coming fromnerbytransmitters is coupled to the antenna, itmay cause intermodulation in the outputtransistors and generate spurs. Inthis case a tuned output filter may be required toremove the problem.

It is mandatory to provide adequate ventilation to the apparatus to maintain its internal temperature as low as possible, in the recommended range $41^{\circ} \mathrm{F}-77^{\circ} \mathrm{F}\left(5 \div 25^{\circ} \mathrm{C}\right)$. Even if the apparatus may sustain $113^{\circ} \mathrm{F}\left(45^{\circ} \mathrm{C}\right)$, and occasionally slightly higher temperatures, his life expectancy will be impaired by high temperature.

As general rule the life expectancy may be halved by each $50^{\circ} \mathrm{F}\left(10^{\circ} \mathrm{C}\right)$ increase in ambient temperature, over $86^{\circ} \mathrm{F}\left(30^{\circ} \mathrm{C}\right)$.

### 3.7 OPERATION

Check that the antenna, the subsequent power amplifier or a suitable dummy load is connected to the amplifierRFoutput. If the NA1001 drives atuned tube amplifier, check that the input of the power amplifier is already tuned on the desired frequency. Control that the power cords are correctly connected to the amplifier and its driver and both the units are off. Before connecting to the amplifier, make sure that the exciter power is set atzero or a very low level ( $<1 \mathrm{~W}$ ) and the frequency is correctly set. Check that the exciter output signal is fed to amplifier input, then:

1) Switch-on the power-on switch on the NA1001:

- the switch will glow red.
- Internal blowers will start.
- NoLEDshould lighton.
- No RF output power should be present.

2) Properly position the meter switch to observe the RF output increasing on the amplifier.
3) Switch-on the power-on switch on the exciter
4) Slowly raise the drive power to the required level, i.e. $10 \div 12 \mathrm{~W}$.

- The RF output power should rise from zero to the nominal 1000 Watt, if the output power adjustment is set is to maximum on the amplifier front panel.
- NoLED should lighton.
- As a general rule, the input power must be $20 \%$ higher than the minimum level required to the full output power (e.g. 12 W if 10 W are enough to obtain 1000 W on the output).

5) Control and note for future reference the correct reading of the operating parameters through the internal instrumentation, which must indicate the following values:

- FORWARD POWER: up to 1000W
- REFLECTED POWER: < 50 W , typ. $0 \div 20 \mathrm{~W}$
- REGULATED VOLTAGE: 48V (300V meter range)
- UNREGULATED VOLTAGE: $140 \mathrm{~V} \pm 15 \%$

Some amplifiers do not permit the reading of the regulated and unregulated voltage on the internal meter.

The installation of the amplifier is thereby completed. A spectrum analysis is now advisable to assure no spurious products due to internal or external causes (i.e. reverse intermodulation on the final stage) are generated. NICOM wishes you success in your work and reminds you that they are always available for further information or to tackle any specific problem.

### 3.8 POSSIBLEMALFUNCIONS

NoLED alarm should be on during regularoperation: following is a list of possible malfunction causes.

## "VSWR" LED on

This LED turns on when the reflected output power exceeds the 70-80 W threshold. In this case, do not operate the system and check antenna, relevant wiring and connectors.

When the amplifier is connected to a successive amplifier, re-tune the latter's input to obtain the smallestreflected power.

This light should never turn on; it might however flash briefly at low power when firstly tuning the input of an NA1001-driven tube amplifier or a cavity band-pass filter.

## "Temperature" LED on

ThisLED turns on when the internal temperature is excessive. Reduce environment temperature and increase room ventilation. In this case, it is important that the hot air released by the unit be exhausted.

Check the regularoperation of the internal ventilationfans andcleanany externally applieddustfilter, ifany.

Since the NA1001 is cooled by air, it is subject to clogging by dust. Because of the high-quality materials used in theirmanufacture, if it is installed as set forth under"INSTALLATIONANDUSE," it will not require special maintenance for quite some time.

A regular service routine, mainly to remove internal dust is suggested over a 6 month to a year period. Keep in mind that $90 \%$ of the aircirculation is restricted to the main internal ventilation channel and does not affect the components. Regularly change the ventilationfan, especially inhigher temperature environments. Change the fanevery 2 years: always use the samehigh quality ball bearing fantype.

After a few years of continuous service, it is recommended that the apparatus be overhauled in the factory or in a specialized laboratory, where the characteristics can be checked against the initial ones and recalibration can be made when needed.

It is also especially important that the power supply be over-hauled when the apparatus has been working at hightemperatures, over $86^{\circ} \mathrm{F}\left(30^{\circ} \mathrm{C}\right)$.

Never change or cause the original settings to be changed when the necessary, complex testing equipment and standard calibration procedures are not available.

5

## WARRANTY

Like all NICOM's solid state equipment, the NA1001 carries a two-year warranty on all its components with the exclusion of the finalRF power module, which may be damaged by faulty output connections.

This warranty is void if the unit is tampered with or if failure is due to improper use, wrong installation or external causes, such as AC overvoltage.

This warranty covers work done exclusively in our laboratories and in those of our agreed representatives.

The goods shall be delivered carriage prepaid to the laboratory and shall be returned freight forward.

This guarantee does not cover any consequential damage due to non-operation or faulty operation.

## SERVICE MANUAL

### 6.1 SYSTEMDESCRIPTION

3 basic sections compose the NA1001: the RF amplifier box, the power supply and the control and metering section.

The RFsection comprises $2 \times 500 \mathrm{~W}$ amplifier modules connected through strip-line combiners. All the RF transistors are Mos-Fettype. A low-pass filter with directional coupler completes the section, which is completely screened by a metal box, to comply withEMI requirements. A fully planardesign permits an immediate access and inspection to the 4 internal modules.

The power supply comprises a mains transformer, whose output is rectified and filtered and a highly efficient Switch-Mode Power Supply regulator.

The RF control section is built on one small board. It performs RF AGC and protection control; providing metering and an interface to the external I/O port. Both direct and reflected power are displayed and provided as proportional analog signals at the Remote I/O port. Through this port is possible, as well, to command the RFoutput power, overcoming the internal front panel regulation.

## 6.2 <br> INTERNAL DESCRIPTION



NA1001: Block diagram

The NA1001 amplifier is composed by 6 internal different modules/boards plus some spare components, as can be seen in the drawing of the inner contents and in the "General wiring diagram"; both comprised in this manual:
-The power supply transformer, rectifier and capacitor
-The Switch Mode Power Supply regulator
-The RF control and measure board
-The input RF power splitter
-The 500W RF power amplifier modules
-The output RF combiner, Low-Pass Filter and coupler

For the detailed description of each module on the following pages, always refer to the corresponding electrical diagram, in the relevant section of the manual.

## NM <br> WARNING!

THIS SECTION IS ONLY AIMED AT GENERAL KNOWLEDGE OF THE UNIT AND FOR THE PURPOSE OF SERVICING THE UNIT BY SKILLED PERSONNEL. AS EXPLAINED IN THE PREVIOUS SECTIONS, INTERNAL ADJUSTMENTS ARE NOT REQUIRED DURING NORMAL OPERATION. TAMPERING WITH INTERNAL SETTINGS VOIDS THE WARRANTY, MAY HARM THE APPARATUS AND JEOPARDIZE THE GUARANTEED PERFORMANCE.

IN ADDITION, MANY MODULES ARE TOO SPECIALIZED AND DIFFICULT TO REPAIR EVEN BY SKILLED TECHNICIANS AND MUST BE REPLACED IN CASE OF NEED BY BRAND NEW ONES AND POSSIBLY RETURNED BACK TO FACTORY TO VERIFY IF THEY CAN BE REPAIRED.

ANY ISPECTION ON THE MODULES DESCRIBED ABOVE MUST BE EXECUTED WITH THE TOP COVER REMOVED AND OFTEN WITH THE OPERATING APPARATUS CONNECTED TO THE POWER. ALTHOUGH MOST OF THE PARTS UNDER VOLTAGE ARE INSULATED AND ARE NOT EASILY ACCESSIBLE, THIS EXPOSES TO THE RISK OF ACCIDENTAL CONTACT WITH THE AC VOLTAGE. TO AVOID IT, ALWAYS USE INSULATED TOOLS AND NEVER TOUCH THE SUPPLY TRANSFORMER, THE POWER SWITCH OR THE POWER SOCKET WITH AC CONNECTORS. NEVER OPERATE THE EQUIPMENT WITH THE COVERS REMOVED. REMOVAL OF THE BOTTOM RF COVER MAY LEAD TO IMPROPER FUNCTIONING OF ANY ELECTRONIC MEASURING METER DUE TO HIGH RF FIELD.

### 6.3 The power supply components

The power supply components, other than the boards below described, are very few: mainly the power transformer with a power relay, a bridge rectifier and a power capacitor, which delivers the raw rectified dc power to the SMPS regulator module.

The unregulated dc voltage, nominally 140 Vdc , may range $120 \div 170 \mathrm{~V}$. The primary tap on the power transformer is factory set on the 230 V input, allowing a mains range approximately $200 \div 250$ Vac. Should the mains voltage be 240 Vac nominally, it is suggested to change the transformer tap to that voltage. If the mains voltage is a stable $215 \div 225 \mathrm{Vac}$, the transformer tap may be left as factory set. Only if there are frequent occasional drops of mains input below 195 V and consequent system stops, it is suggested to lower the input tap to 220 V .

To do that, the power cord must be disconnected from the mains, the top cover must be removed and the transformer voltage terminals may be accessed.

An USA version is provided with a someway different transformer and general wiring (see the appropriate electrical diagram and internal layout). In this version, some jumpers must be preset on the equipment's internal terminal board TB1 to provide 115 or 230Vac operation, if not factory wired. In details these settings are:

## 220 Vac 1/P3 to 3/P4 <br> 115 Vac $\quad 3 / \mathrm{P} 3$ to 3/P4 and $1 / \mathrm{P} 3$ to 1/P4

### 6.4 TheSwitch Mode PowerSupply regulator

This module performs an efficient regulation of the raw dc input, nominally $140 \mathrm{~V} \pm 15 \%$ to a lower $48 \mathrm{~V} \pm 1 \%$. Being its efficiency very high, very little heat is produced in the regulation process. The nominal current capability of the regulator is much higher than requested, and approaches 40A @ 48V.

A control I/O connector on an upper daughter board permits a remote control of the regulator

NA1001:
Positioning of the power supply internal terminal board


### 6.4 The Switch Mode Power Supply regulator

This module performs an efficient regulation of the raw DC input, nominally $140 \mathrm{~V} \pm 15 \%$ to a lower $48 \mathrm{~V} \pm 1 \%$. Being its efficiency very high, very little heat is produced in the regulation process. The nominal current capability of the regulator is much higher than requested, and approaches 70A @ 48V.

A control I/O connector on an upper daughter board permits a remote control of the regulator by the apparatus controller, i.e. output on/stand-by, current and voltage monitoring, status prompting and alert.

A fast 80A semiconductor-grade protection fuse is screwed on the board: it may be fused by the crowbar protection in case of switching transistor damage. If this happens verify the integrity of the power transistor before attempting to replace the fuse. Usually something is broken , causing the fuse to blow-up.

Fixing this module in the field is very difficult if any component other than the fuse and/or a power transistor failed. We suggest substituting the module with a new one and sending back the damaged unit to the factory for inspection and possible repair.

### 6.5 The RF control and measure board

This small board carries all the circuitry to control and protect the RF amplifier stage. Let us consider its various loops.

Two identical buffers, IC4a and IC3a, insulate and amplify the direct and reflected signal detected on the RF output coupler, with different gain. The main direct power regulator loop is built around the subsequent IC4d op-amp, which compares the sensed signal with the preset power level on RT5. Adjusting this trimmer, the RF output power may be varied to values different from that factory preset. Never exceed a safe 1000 W on RF output, even if the amplifier is usually able to easily go over this limit, to have some safety margin. The output of IC4d constitutes the AGC line, which is buffered by IC5 to drive the RF transistor gates. Both the two sections of IC5 are in parallel to increase the current capability of the external AGC line.

The reflected power protection is managed by IC3c, which compares the reflected sensed signal to a fixed threshold, which is set to $70 / 80 \mathrm{~W}$, as determined by R35 and R36. The output of IC3 adds on the internal AGC line though D14. The action of this circuit is proportional: i.e. the output power is continuously decreased till the fraction which is reflected back no more exceeds the safe maximum level. There is no RF complete switch off even with severe load mismatch.

Both direct and reflected signal lines are conveyed to the remote connector through insulating 10kohm resistors

The temperature protection on the output stage is performed by IC4b, which trips when the temperature sense line crosses its preset threshold, completely disabling the RF output. The temperature sensor is mounted on the heatsink, near the RF transistors, and is constitued by a precise PTC resistors, which varies its resistance accordingly to the temperature.

On this board a small negative rectifier and a regulator (TR5) provides the negative bias to completely disable the RF power, if needed. The positive regulator TR4 derives the positive 11.3 V board supply from the +48 V regulated line.

### 6.6 The input RF power splitter

The purpose of this simple board is mainly to divide the input RF drive power in two identical signals, one for each power amplifier module, providing a good insulation between each output port ( $>20 \mathrm{~dB}$, typ. 23 dB minimum on the whole FM band).

This is done by a Wilkinson type printed coupler, followed by the balancing resistor array $\mathrm{R} 21 \div \mathrm{R} 24$.

A directional coupler senses the input RF level and RT1 is regulated to provide the overdrive protection circuit trip at the right maximum input level. The board also supports the forward and reflected detector sensitivity trimmers, whose input comes from the output board.

Two additional lines support the RF module bias (or AGC) line and the temperature sensing PTC thermistor.

### 6.7 The RF power amplifier modules

These modules are built around a couple of "Gemini type" Mos-fet transistors each one forming a 300W push-pull amplifier.

Discrete Wilkinson-type couplers equip both the input and the output module section, doing the job of dividing and recombining the input and output signals, providing a suitable insulation between the transistors.

A small balancing resistor R 1 is mounted on the input splitter, while a much bigger resistor R14 is mounted in the output combiner.

A group of C, R and L RF decoupler and dampening components are mounted on the positive supply line of each amplifier, plus a small value resistor, R12 and R13, for possible separate current detection of each supply leg.

The gate bias is separately adjusted through R15 and R16 on each section. Do not tamper with the factory bias preset values!

The full power output of the whole module exceeds 600 W , to provide some room for coupling losses on the combining stages of higher power amplifiers, like the same NA1001.

### 6.8 The output RF power combiner, LPF and coupler

This module is symmetric to the input power splitter and is another printed Wilkinson coupler, whose power management capability is obviously much higher than the input board. In this case the power balancing resistors are high power devices, whose centre connection is referred to ground through an inductor, which discharges any static electricity on the antenna up to a relevant amount of power.

The power combiner is followed by a printed low-pass filter, which attenuates the harmonic products generated by the amplifiers.

3 directional sample lines derive two rectified voltages proportional to the direct and reflected output power and a RF signal for external monitoring purposes.

## 7 REPAIR AND REPLACEMENT OF DAMAGED MODULES

The NA1001 is a highly reliable unit,due to the excellent design and development done to assure the maximum reasonable working margin for each part. Nevertheless, with all units which work 24 hours a day for years, some failures are possible, especially in those environments which over-stress the apparatus, like hot or dusty or moist places, or those subjected to wide power fluctuations or static discharges, etc.

In the event of any failure an appropriate analysis must be done to avoid subsequent failures due to faulty ambient conditions. An often underestimates cause of failure is simply a too high ambient temperature or insufficient ventilation. Improving the ambient and system ventilation as suggested in the installation paragraph of this manual, usually fixes the problem.

Other obvious causes may be dust clogging and ventilator fan failure. A regular service and maintenance routine will avoid these sources of problems and we suggest changing the ventilator every two years, even if no damage is visible, especially at high ambient temperature.

If a pipe is added to extract air, then an additional fan is required to help air flow.
In any case, if the amplifier fails, some work can be done on the unit to fix the problem. With the appropriate spare parts, most of repair may be done on site, without need of special tools and often without need of any solder joint.

In general very little need be said about changing board components: virtually all of them may be changed in few minutes, without retouching the adjustments. Most of them are immediately accessible or need a minimum of dislocation of other components and plates. Only the RF boards require more work.

RF boards are delicate modules, which contain some parts as flanged power transistors and resistors which must separately be screwed on the supporting heatsink and may be easily damaged by improper handling. These boards are the 500 W power amplifier modules and the RF output combiner.

Repairs of these modules are usually made in the factory or in a specialized laboratory, if possible at all. If the p.c. board is damaged perhaps only the costly RF active devices may be recovered. Nevertheless, very often this is worthless because, in the case of major damage, these parts are internally electrically damaged or degraded.

Repair of the RF modules requires too, at the end of the reparation, a full check of the module's working parameters in a dummy fixture or in a test assembly which are not available even in most specialized laboratories. Because of this repair of the modules, especially the higher power amplifiers, is mostly discouraged and the broken one must be replaced by new parts with the same identical characteristics, fully tested at the factory.

To replace the modules avoiding as much as possible to damage the new part or the old transistors, if not already broken, carefully follow the subsequent steps:

1) Remove the amplifier cabinet from the rack, after having disconnected from its rear connectors the RF input and output cables, the power supply and the control cables. Disconnect also the ground cable from its screw.
2) To investigate the damaged parts or to test the repair,one must externally connect the removed cables and the RF output load to the amplifier assembly in a manner to allow inner inspection of the top and bottom of the unit. If the latter is placed on a small stand next to the main rack, the internal cables are usually long enough to allow the connections, avoiding extension cables.
3) Open the bottom cover of the cabinet and remove the screen from the damaged module(s), if any.
4) If the damage is not immediately visible, it may be helpful to measure the currents sunk by each 300 W sub-module amplifier. To this aim a low ohmic value shunt resistor is inserted in series to the 48 V power supply of the module's subsections (R12 and R13, 10m $\Omega$ ). To measure the current sunk, the amplifier assembly must be completely connected and powered with and without RF. A sensitive, RF proof, digital voltmeter must be used to measure the voltage across the shunt resistors, which vary from nearly 1 mV at no load to 100 mV at full power.
Take care: most of low quality digital or analog meters are not able to do this reading, because they are affected by the high RF field and their reading is completely meaningless! WARNING: great care must be paid not to accidentally short-circuit the resistor leads to the ground with the voltmeter probe tips, during the measurements!
5) When properly functioning at full power, each module 300 W subsection will sink $8 \div 10$ Amperes, i.e. $80 \div 100 \mathrm{mV}$ across the shunt resistor. The absorption must be balanced $\pm 10 \%$ around the mean value on each amplifier. A lower or higher value may mean a module failure.
6) Remove the power supply cable screwed on a centre terminal in the board and the small bias cable.
7) Unscrew the input and output RF connections, at the module opposite sides.
8) Carefully unscrew the RF transistor flanges from the heatsink base-plate. This operation, if not properly done, may mechanically over-stress the transistor, cracking the internal delicate beryllium-oxide ceramic which supports the active silicon dies and determine unrecoverable damage of the device.
CAUTION: beryllium-oxide is toxic and must not be thrown with domestic refuse but in
specialised toxic material disposals. No special handling precaution must be paid when the transistors or power resistors are not mechanically broken, apart those deriving from the handling of mechanically fragile (and very costly) devices. If the transistor or resistor flange is broken, avoid touching it or the brittle white exposed internal ceramic or inhaling the dust from it. Dispose of the transistor or the entire broken module as previously described.
9) Make a note of the position and the length and remove the threaded screen spacers and the board fixing screws.
10)Remove the broken module and clean the supporting heatsink base-plate before mounting the new one.
11)Smear thin heat-conductive silicon grease below the flanges of the power transistors and resistors of the new module, before mounting it.
12)Position the new module, placing the threaded spacers and screws over the p.c. board avoid tightening them. When all the screws are placed, correctly align the transistors and resistors fixing holes and tighten the screws and spacers.
10) Insert the proper screws and washers, if any, across the transistors and resistors and carefully tighten them in several, alternate steps.
11) Reconnect the power supply and bias cables to the module.
12) Turn-on the amplifier fully connected but without RF power, with RF load connected and driver exciter off. Enable the equipment, with the exciter still off.
13) Measure the bias current of the two transistors on the module, as explained on previous paragraphs 4 and 5. They were factory adjusted to 100 mA ( 1 mV ).
17)If the currents are off the range $50 \div 200 \mathrm{~mA}(0.5 \div 2 \mathrm{mV})$, carefully retouch the bias trimmers on the board. A small clockwise rotation increases the bias current.
14) Reduce the output power setting to a low value, acting on the front panel power set trimmer and turn on the exciter power.
15) Slowly increase the power and measure the balance of the current drained by each module at half level and at full power. Verify the limits written in paragraph 5.
16) Turn off the equipment, reassemble the screening covers and the bottom panel of the apparatus and reposition it in its working location with full connections.
17) Perform a limited testing period at full power, i.e. $1050 \div 1100 \mathrm{~W}$ and then reduce power at maximum nominal working level, i.e. no more than 1000 W .

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## NA1001 AMPLIFIER - FRONT \& TOP INTERNAL VIEW



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\text { p. } 25
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NA1001 AMPLIFIER - REAR \& BOTTOM INTERNAL VIEW


## NA 1001 AMPLIFIER - ELECTRICAL DIAGRAM (220-240Vac) CONTROLS \& MEASURES BOARD




## NA1001- USER AND MAI NTENANCE MANUAL - NicomUsa, Inc

 NA 1001 AMPLIFIER - POWER SUPPLY FRONT-END

p. 30

## SRFB1K0AL2 - RF CONTROLS \& MEASURES BOARD COMPONENT LAYOUT



p. 31

## SRFB1K5ALM - 48V/40A SMPS REGULATOR ELECTRICAL DIAGRAM - POWER SECTION



SRFB1K5ALM - 48V/40A SMPS REGULATOR ELECTRICAL DIAGRAM - CONTROL SECTION

p. 33

SRFB1K5ALM - 48V/40A SMPS REGULATOR


SRFB1K5ALM - 48V/40A SMPS REGULATOR COMPONENT LAYOUT - CONTROL SECTION


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## SRFB1K0IN - 2-PORT RF INPUT SPLITTER ELECTRICAL DIAGRAM



## SRFB1K0PB - 2-PORT RF OUTPUT COMBINER \& LPF ELECTRICAL DIAGRAM



## SRFB500W - 500W AMPLIFIER MODULE ELECTRICAL DIAGRAM



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## SRFB500W - 500W AMPLIFIER MODULE COMPONENT LAYOUT



## SRFB1K0AL2 - RF CONTROLS AND MEASURES BOARD

## REF.

C24
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## C18

C19
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C5
C40
C33
C30
C36
C37
C43
C29
C38
C47
D17
D13,
D14,
D15
D16
D4
D5
IC5
IC3
IC4
P1 12 POLES
P2 5 POLES
R16
R5
R57
R58
R31
R61
R62
R33
R34
R45
R47
R48
R3

## DESCRIPTION

CAPACITOR CERAMIC 100pF 2\% 100V NP0 P5 CAPACITOR CERAMIC 100pF 2\% 100V NPO P5 CAPACITOR CERAMIC 100pF 2\% 100V NP0 P5 CAPACITOR CERAMIC 100pF 2\% 100V NP0 P5 CAPACITOR CERAMIC 100pF 2\% 100V NPO P5 CAPACITOR CERAMIC $1 \mathrm{nF} 5 \% 50 \mathrm{~V}$ P2,5 TC

CAPACITOR CERAMIC 1nF 5\% 50V P2,5 TC
CAPACITOR CERAMIC $1 \mathrm{nF} 5 \% 50 \mathrm{~V}$ P2,5 TC
CAPACITOR CERAMIC $1 \mathrm{nF} 5 \% 50 \mathrm{~V}$ P2,5 TC
CAPACITOR CERAMIC $1 \mathrm{nF} 5 \% 50 \mathrm{~V}$ P2,5 TC
CAPACITOR CERAMIC $1 \mathrm{nF} 5 \% 50 \mathrm{~V}$ P2,5 TC
CAPACITOR CERAMIC $1 \mathrm{nF} 5 \% 50 \mathrm{~V}$ P2,5 TC
CAPACITOR CERAMIC $1 \mathrm{nF} 5 \% 50 \mathrm{~V}$ P2,5 TC
CAPACITOR CERAMIC $1 \mathrm{nF} 5 \% 50 \mathrm{~V}$ P2,5 TC
CAPACITOR CERAMIC $1 \mathrm{nF} 5 \% 50 \mathrm{~V}$ P2,5 TC
CAPACITOR CERAMIC $1 \mathrm{nF} 5 \% 50 \mathrm{~V}$ P2,5 TC
CAPACITOR ELECTROLITC VERT. $105^{\circ} \mathrm{C} 100 \mu \mathrm{~F} 25 \mathrm{~V}$ D8
CAPACITOR ELECTROLITC VERT. $105^{\circ} \mathrm{C} 220 \mu \mathrm{~F} 35 \mathrm{~V}$ D10
CAPACITOR POLYESTER 1,0nF 10\% 100V P5
CAPACITOR POLYESTER 2,2nF 10\% 100V P5
CAPACITOR POLYESTER 4,7nF 10\% 100V P5
CAPACITOR POLYESTER 100nF 10\% 63V P5
CAPACITOR POLYESTER 100nF 10\% 63V P5
CAPACITOR POLYESTER 470nF 10\% 63V P5
CAPACITOR TANTALIUM $2,2 \mu \mathrm{~F} 25 \mathrm{~V}$ P5
CAPACITOR TANTALIUM 4,7 $\mu \mathrm{F}$ 16V P5
CAPACITOR TANTALIUM $4,7 \mu \mathrm{~F}$ 16V P5
DIODE RECTIFIER 1N4004 SI 1A 400V
DIODE SIGNAL 1N4148 SI DO 35
DIODE SIGNAL 1N4148 SI DO 35
DIODE SIGNAL 1N4148 SI DO 35
DIODE SD103A SI SCHOTTKY RECT. 40V 0,5A
DIODE ZENER 1068 400mW 6,8V DO 35
DIODE ZENER 1112 400mW 12V DO 35
INTEGRATED CIRC. NE5532 DIP8 2-LOW NOISE OP.AMP
INTEGRATED CIRC. TLC274 DIP14 4-LCMOS OP.AMP
INTEGRATED CIRC. TLC274 DIP14 4-LCMOS OP.AMP
PIN STRIP 2,54 M 6x6 DIR.20040 POLES 18
PIN STRIP 2,54 M 6x6 DIR.20040 POLES 18
RESISTOR RS2F/100 10.0 OHM 1/2W 1\% 1
RESISTOR RS2F/475 47.5 OHM 1/2W 1\%
RESISTOR RS2F0100 100 OHM 1/2W 1\%
RESISTOR RS2F0100 100 OHM 1/2W 1\%
RESISTOR RS2F0412 412 OHM 1/2W 1\%
RESISTOR RS2F0619 619 OHM 1/2W 1\%
RESISTOR RS2F0619 619 OHM 1/2W 1\%
RESISTOR RS2F0681 681 OHM 1/2W 1\%
RESISTOR RS2F1100 1.00K OHM 1/2W 1\%
RESISTOR RS2F1150 1.50K OHM 1/2W 1\%
RESISTOR RS2F1150 1.50K OHM 1/2W 1\%
RESISTOR RS2F1150 1.50K OHM 1/2W 1\%
RESISTOR RS2F1182 1.82K OHM 1/2W 1\%
Q.TY

R52
R29
R30
R32
R38
R23
R24
R46
R56
R54
R25
R26
R37
R43
R49
R50
R51
R59
R60
R22
R2
R35
R39
R28
R36
R40
R55
R27
R53
RT1
RT3
RT4
RT5
TR4
TR5
for TR4
for IC5
for IC3, IC4
for IC3, IC4

RESISTOR RS2F1280 2.80K OHM 1/2W 1\%
RESISTOR RS2F1332 3.32K OHM 1/2W 1\%
RESISTOR RS2F1332 3.32K OHM 1/2W 1\%
RESISTOR RS2F1332 3.32K OHM 1/2W 1\%
RESISTOR RS2F1332 3.32K OHM 1/2W 1\%
RESISTOR RS2F1475 4.75K OHM 1/2W 1\%
RESISTOR RS2F1475 4.75K OHM 1/2W 1\%
RESISTOR RS2F1475 4.75K OHM 1/2W 1\%
RESISTOR RS2F1475 4.75K OHM 1/2W 1\%
RESISTOR RS2F1619 6.19K OHM 1/2W 1\%
RESISTOR RS2F2100 10.0K OHM 1/2W 1\%
RESISTOR RS2F2100 10.0K OHM 1/2W 1\%
RESISTOR RS2F2100 10.0K OHM 1/2W 1\%
RESISTOR RS2F2100 10.0K OHM 1/2W 1\%
RESISTOR RS2F2100 10.0K OHM 1/2W 1\%
RESISTOR RS2F2100 10.0K OHM 1/2W 1\%
RESISTOR RS2F2100 10.0K OHM 1/2W 1\%
RESISTOR RS2F2100 10.0K OHM 1/2W 1\%
RESISTOR RS2F2100 10.0K OHM 1/2W 1\%
RESISTOR RS2F2110 11.0K OHM 1/2W 1\%
RESISTOR RS2F2140 14.0K OHM 1/2W 1\%
RESISTOR RS2F2221 22.1K OHM 1/2W 1\%
RESISTOR RS2F2221 22.1K OHM 1/2W 1\%
RESISTOR RS2F2332 33.2K OHM 1/2W 1\%
RESISTOR RS2F2475 47.5K OHM 1/2W 1\%
RESISTOR RS2F3100 100K OHM 1/2W 1\%
RESISTOR RS2F3110 110K OHM 1/2W 1\%
RESISTOR RS2F3221 221K OHM 1/2W 1\%
RESISTOR RS2F3475 475K OHM 1/2W 1\%
TRIMMER HORIZ. CERAM. RES. Q10 110-1K OHM
TRIMMER HORIZ. CERAM. RES. Q10 210-10K OHM
TRIMMER HORIZ. CERAM. RES. Q10 210-10K OHM
TRIMMER HORIZ. CERAM. RES. Q10 310-100K OH
TRANSISTOR 2N1711 TO5 60V 1A NPN GEN.P
TRANSISTOR BC556B TO92 65V.1A PNP GEN.P
TRANSISTOR SPACER TO5 4mm NYLON

SOCKET DIL08 LOW PROFILE - I=7,62

## REF.

C21
C1
C2
C3
C4
C5
C6
C7
C13
C8
D1
L1
L2
L3
L4
L5
P1
R8
R1
R2
R6
R7
R3
R4
R5
R21
R22
R23
R24
RT1
RT2
RT3
RVT1

SRFB1KOIN - 2-PORT INPUT SPLITTER DESCRIPTION
Q.TY

RFB1001 INPUT SPLITTER BOARD
CAPACITOR CHIP CERAM. 1206 6,8pF 5\% 100V NPO 1
CAPACITOR CHIP CERAM. 1206 33pF 5\% 100V NPO 1
CAPACITOR CHIP CERAM. 1206 100pF 5\% 100V NPO 1
CAPACITOR CHIP CERAM. 1206 100pF 5\% 100V NPO 1
CAPACITOR CHIP CERAM. 1206 100pF 5\% 100V NPO 1
CAPACITOR CHIP CERAM. 1206 100pF 5\% 100V NPO 1
CAPACITOR CHIP CERAM. 1206 100pF 5\% 100V NPO 1
CAPACITOR CHIP CERAM. 1206 1,0nF 10\% 100V NPO 1
CAPACITOR CHIP CERAM. 1206 1,0nF 10\% 100V NPO 1
CAPACITOR CHIP CERAM. 1206 100nF 10\% 50V X7R 1
DIODE BAT54S SOT23 DUAL SCHOTTKY .2A/30 1
INDUCTOR CHIP 1210 1.0UH LO-Q 1
INDUCTOR CHIP 1210 1.0UH LO-Q 1
INDUCTOR CHIP 1210 1.0UH LO-Q 1
INDUCTOR CHIP 1210 1.0UH LO-Q 1
INDUCTOR CHIP 1210 1.0UH LO-Q 1
MALE CONNECTOR C.S. FLAT CABLE 10p 1
RESISTOR CHIP 120656 OHM 1/4W 1\% 1
RESISTOR CHIP 1206120 OHM 1/4W 1\% 1
RESISTOR CHIP 1206 1.0K OHM 1/4W 1\% 1
RESISTOR CHIP 1206 1.0K OHM 1/4W 1\% 1
RESISTOR CHIP 1206 1.0K OHM 1/4W 1\% 1
RESISTOR CHIP 1206 10K OHM 1/4W 1\% 1
RESISTOR CHIP 1206 10K OHM 1/4W 1\% 1
RESISTOR CHIP 1206 10K OHM 1/4W 1\% 1
RESISTOR CHIP 2512100 OHM 1W 5\% 1
RESISTOR CHIP 2512100 OHM 1W 5\% 1
RESISTOR CHIP 2512100 OHM 1W 5\% 1
RESISTOR CHIP 2512100 OHM 1W 5\% 1
TRIMMER RES.CERMET SMD 5x5 20k OHM G4BT 1
TRIMMER RES.CERMET SMD $5 \times 5$ 20k OHM G4BT 1
TRIMMER RES.CERMET SMD $5 \times 5$ 20k OHM G4BT 1
RESISTOR PTC TO92 2,kOHM 25º ¹\% 64-52-54

| REF. | DESCRIPTION | Q.ty |
| :---: | :---: | :---: |
| C 1 | CAPACITOR, CERAMIC M.S. $0,22 \mathrm{MF}$ 50V P.5.08 X7R | 1 |
| C 7 | CAPACITOR, CERAMIC M.S. 470 PF 50 V P. 2.54 NPO | 1 |
| C59 | CAPACITOR, CERAMIC M.S. 470 PF 50 V P. 2.54 NPO | 1 |
| C86 | CAPACITOR, CERAMIC M.S. 470 PF 50 V P. 2.54 NPO | 1 |
| C2 | CAPACITOR, CERAMIC M.S. 10000 PF 50V P. 2.54 X7R- | 1 |
| C3 | CAPACITOR, CERAMIC M.S. 10000 PF 50V P.2.54 X7R- | 1 |
| C4 | CAPACITOR, CERAMIC M.S. 10000 PF 50V P. 2.54 X7R- | 1 |
| c9 | CAPACITOR, CERAMIC M.S. 10000 PF 50V P. 2.54 X7R- | 1 |
| C15 | CAPACITOR, CERAMIC M.S. 10000 PF 50V P. 2.54 X7R- | 1 |
| C25 | CAPACITOR, CERAMIC M.S. 10000 PF 50V P.2.54 X7R- | 1 |
| C26 | CAPACITOR, CERAMIC M.S. 10000 PF 50V P. 2.54 X7R- | 1 |
| C29 | CAPACITOR, CERAMIC M.S. 10000 PF 50V P. 2.54 X7R- | 1 |
| C32 | CAPACITOR, CERAMIC M.S. 10000PF 50V P. 2.54 X7R- | 1 |
| C39 | CAPACITOR, CERAMIC M.S. 10000 PF 50V P. 2.54 X7R- | 1 |
| C40 | CAPACITOR, CERAMIC M.S. 10000 PF 50V P.2.54 X7R- | 1 |
| C42 | CAPACITOR, CERAMIC M.S. 10000 PF 50V P. 2.54 X7R- | 1 |
| C43 | CAPACITOR, CERAMIC M.S. 10000 PF 50V P. 2.54 X7R- | 1 |
| C45 | CAPACITOR, CERAMIC M.S. 10000 PF 50V P. 2.54 X7R- | 1 |
| C51 | CAPACITOR, CERAMIC M.S. 10000 PF 50V P.2.54 X7R- | 1 |
| C55 | CAPACITOR, CERAMIC M.S. 10000 PF 50V P.2.54 X7R- | 1 |
| C56 | CAPACITOR, CERAMIC M.S. 10000 PF 50V P. 2.54 X7R- | 1 |
| C57 | CAPACITOR, CERAMIC M.S. 10000 PF 50V P. 2.54 X7R- | 1 |
| C71 | CAPACITOR, CERAMIC M.S. 10000 PF 50V P. 2.54 X7R- | 1 |
| C73 | CAPACITOR, CERAMIC M.S. 10000 PF 50 V P.2.54 X7R- | 1 |
| C76 | CAPACITOR, CERAMIC M.S. 10000 PF 50V P. 2.54 X7R- | 1 |
| C77 | CAPACITOR, CERAMIC M.S. 10000 PF 50V P.2.54 X7R- | 1 |
| C81 | CAPACITOR, CERAMIC M.S. 10000 PF 50V P. 2.54 X7R- | 1 |
| C82 | CAPACITOR, CERAMIC M.S. 10000PF 50V P.2.54 X7R- | 1 |
| C 5 | CAPACITOR, CERAMIC M.S. 1000PF 50V P. 2.54 NPO | 1 |
| C14 | CAPACITOR, CERAMIC M.S. 1000PF 50V P. 2.54 NPO | 1 |
| C20 | CAPACITOR, CERAMIC M.S. 1000PF 50V P. 2.54 NPO | 1 |
| C21 | CAPACITOR, CERAMIC M.S. 1000PF 50V P. 2.54 NPO | 1 |
| C22 | CAPACITOR, CERAMIC M.S. 1000 PF 50 V P. 2.54 NPO | 1 |
| C23 | CAPACITOR, CERAMIC M.S. 1000 PF 50 V P.2.54 NPO | 1 |
| C24 | CAPACITOR, CERAMIC M.S. 1000 PF 50 V P.2.54 NPO | 1 |
| C28 | CAPACITOR, CERAMIC M.S. 1000 PF 50 V P.2.54 NPO | 1 |
| C31 | CAPACITOR, CERAMIC M.S. 1000 PF 50 V P. 2.54 NPO | 1 |
| C33 | CAPACITOR, CERAMIC M.S. 1000 PF 50 V P.2.54 NPO | 1 |
| C34 | CAPACITOR, CERAMIC M.S. 1000 PF 50 V P.2.54 NPO | 1 |
| C36 | CAPACITOR, CERAMIC M.S. 1000 PF 50 V P.2.54 NPO | 1 |
| C44 | CAPACITOR, CERAMIC M.S. 1000 PF 50 V P.2.54 NPO | 1 |
| C52 | CAPACITOR, CERAMIC M.S. 1000 PF 50 V P.2.54 NPO | 1 |
| C58 | CAPACITOR, CERAMIC M.S. 1000 PF 50 V P. 2.54 NPO | 1 |
| C65 | CAPACITOR, CERAMIC M.S. 1000 PF 50 V P. 2.54 NPO | 1 |
| C67 | CAPACITOR, CERAMIC M.S. 1000 PF 50 V P. 2.54 NPO | 1 |
| C70 | CAPACITOR, CERAMIC M.S. 1000 PF 50 V P. 2.54 NPO | 1 |
| C80 | CAPACITOR, CERAMIC M.S. 1000PF 50V P. 2.54 NPO | 1 |
| C83 | CAPACITOR, CERAMIC M.S. 1000 PF 50 V P.2.54 NPO | 1 |
| C6 | CAPACITOR, CERAMIC M.S. 100PF 50V P. 2.54 NPO | 1 |

CAPACITOR, CERAMIC M.S. 100PF 50V P.2.54 NPO

CAPACITOR, CERAMIC M.S. 100PF 50V P. 2.54 NPO CAPACITOR, CERAMIC M.S. 100PF 50V P.2.54 NPO CAPACITOR, CERAMIC M.S. 100PF 50V P. 2.54 NPO CAPACITOR, CERAMIC M.S. 100PF 50V P. 2.54 NPO CAPACITOR, CERAMIC M.S. 100PF 50V P. 2.54 NPO CAPACITOR, CERAMIC M.S. 100PF 50V P. 2.54 NPO CAPACITOR, CERAMIC M.S. 100PF 50V P. 2.54 NPO CAPACITOR, CERAMIC M.S. 100PF 50V P. 2.54 NPO CAPACITOR, CERAMIC M.S. 100PF 50V P. 2.54 NPO CAPACITOR, CERAMIC M.S. 100PF 50V P. 2.54 NPO CAPACITOR, CERAMIC M.S. 100PF 50V P. 2.54 NPO CAPACITOR, CERAMIC M.S. 100PF 50V P.2.54 NPO CAPACITOR, CERAMIC M.S. 100PF 50V P. 2.54 NPO CAPACITOR, CERAMIC M.S. 100PF 50V P. 2.54 NPO CAPACITOR, CERAMIC M.S. 100PF 50V P. 2.54 NPO CAPACITOR, CERAMIC M.S. 2200PF 50V P. 2.54 NPO CAPACITOR, CERAMIC M.S. 2200PF 50V P. 2.54 NPO CAPACITOR, CERAMIC M.S. 2200PF 50V P.2.54 NPO CAPACITOR, CERAMIC M.S. 1 MF 50V P.5.08 Z5U CAPACITOR, CERAMIC M.S. 1MF 50V P.5.08 Z5U CAPACITOR, CERAMIC M.S. 1 MF 50 V P.5.08 Z5U CAPACITOR, CERAMIC M.S. 1 MF 50 V P. $5.08 \mathrm{Z5U}$ CAPACITOR, CERAMIC M.S. 1 MF 50V P. $5.08 \mathrm{Z5U}$ CAPACITOR, CERAMIC M.S. 1 MF 50V P. $5.08 \times 7 R$ CAPACITOR, CERAMIC M.S. 1 MF 50V P.5.08 X7R CAPACITOR, CERAMIC M.S. 1 MF 50V P.5.08 X7R CAPACITOR, CERAMIC M.S. 1 MF 50V P.5.08 X7R CAPACITOR, CERAMIC M.S. 1 MF 50V P.5.08 X7R CAPACITOR, CERAMIC M.S. 1 MF 50V P.5.08 X7R DIODE BZX55C16
DIODE BZX55C4V7
DIODE BZX55C4V7
DIODE BZX55C33
DIODE BAV21
DIODE BAV21
DIODE BAV21
DIODE BAV21
DIODE BAV21
DIODE BZX55C18
DIODE SCHOTTKY BAT43/BAT48
DIODE SCHOTTKY BAT43/BAT48
DIODE SCHOTTKY BAT43/BAT48
DIODE SCHOTTKY BAT43/BAT48
DIODE SCHOTTKY BAT43/BAT48
DIODE BZX55C15
I.C.SFH 610A-3
I.C.SFH 610A-3
I.C.SFH 610A-3
I.C.SFH 610A-3
I.C.SFH 610A-3

PRINTED CIRCUIT
CONNECTOR STRAIGHT 16P. 2,54 L.P.
CONNECTOR STRAIGHT 9P. 2.54 L.P.
CONNECTOR FLAT $2 x 7$ WAYS STRAIGHT 2,54 L.P.
BC 327
BC 337

BC 337
MOSFET IRDFD9120
RESISTOR S.M. 220 1/2W P. 10
RESISTOR S.M. 220 1/2W P. 10
RESISTOR S.M. 220 1/2W P. 10
RESISTOR S.M. 330 1/2W P. 10
RESISTOR S.M. 330 1/2W P. 10
RESISTOR S.M. 1K 1/2W P. 10
RESISTOR S.M. 1K 1/2W P. 10
RESISTOR S.M. 470 1/4W P. 6.35
RESISTOR S.M. 470 1/4W P. 6.35
RESISTOR S.M. 470 1/4W P. 6.35
RESISTOR S.M. 11K 1/4W P. 6.35
RESISTOR S.M. 220K 1/4W P. 6.35
RESISTOR S.M. 220K 1/4W P. 6.35
RESISTOR S.M. 220K 1/4W P.6.35
RESISTOR S.M. 2K2 1/4W P. 6.35
RESISTOR S.M. 2K2 1/4W P. 6.35
RESISTOR S.M. 2K2 1/4W P. 6.35
RESISTOR S.M. 2K2 1/4W P. 6.35
RESISTOR S.M. 2K2 1/4W P. 6.35
RESISTOR S.M. 2K2 1/4W P. 6.35
RESISTOR S.M. 2K2 1/4W P. 6.35
RESISTOR S.M. 2K2 1/4W P. 6.35
RESISTOR S.M. 2K2 1/4W P. 6.35
RESISTOR S.M. 2K2 1/4W P. 6.35
RESISTOR S.M. 2K2 1/4W P. 6.35
RESISTOR S.M. 2K2 1/4W P. 6.35
RESISTOR S.M. 27 1/4W P. 6.35
RESISTOR S.M. 9K1 1/4W P. 6.35
RESISTOR S.M. 100 1W 1\% P. 10
RESISTOR S.M. 100 1W 1\% P. 10
RESISTOR S.M. 1K2 1/4W P. 6.35
RESISTOR S.M. 1K2 1/4W P. 6.35
RESISTOR S.M. 1K2 1/4W P. 6.35
RESISTOR S.M. 1K2 1/4W P. 6.35
RESISTOR S.M. 3K3 1/4W P. 6.35
RESISTOR S.M. 3K3 1/4W P. 6.35
RESISTOR S.M. 2K7 1/4W P. 6.35
RESISTOR S.M. 2K7 1/4W P. 6.35
RESISTOR S.M.470K 1/4W P. 6.35
RESISTOR S.M.470K 1/4W P. 6.35
RESISTOR S.M.470K 1/4W P.6.35
RESISTOR S.M. 2M2 1/4W P. 6.35
RESISTOR S.M. 1K 1/4W P. 6.35
RESISTOR S.M. 1K 1/4W P. 6.35
RESISTOR S.M. 1K 1/4W P. 6.35
RESISTOR S.M. 1K 1/4W P.6.35
RESISTOR S.M. 1K 1/4W P.6.35
RESISTOR S.M. 1K 1/4W P.6.35
RESISTOR S.M. 1K 1/4W P.6.35
RESISTOR S.M. 1K 1/4W P.6.35
RESISTOR S.M. 1K 1/4W P.6.35
RESISTOR S.M. 5K1 1/4W P. 6.35
RESISTOR S.M. 1K6 1/4W P. 6.35
RESISTOR S.M. 75 1/4W P. 6.35
RESISTOR S.M. 43K 1/4W P.6.35

R38




RESISTOR S.M. 4K3 1/4W P.6.35
RESISTOR S.M. 4K7 1/4W P. 6.35
RESISTOR S.M. 4K7 1/4W P. 6.35
RESISTOR S.M. 4K7 1/4W P. 6.35
RESISTOR S.M. 4K7 1/4W P. 6.35
RESISTOR S.M. 4K7 1/4W P. 6.35
RESISTOR S.M. 4K7 1/4W P. 6.35
RESISTOR S.M. 4K7 1/4W P. 6.35
RESISTOR S.M. 22K 1/4W P.6.35
RESISTOR S.M. 22K 1/4W P.6.35
RESISTOR S.M. 22K 1/4W P.6.35
RESISTOR S.M. 220 1/4W P. 6.35
RESISTOR S.M. 22 1/4W P. 6.35
RESISTOR S.M. 22 1/4W P.6.35
RESISTOR S.M. 10K 1/4W P. 6.35
RESISTOR S.M. 10K 1/4W P. 6.35
RESISTOR S.M. 10K 1/4W P. 6.35
RESISTOR S.M. 100K 1/4W P. 6.35
RESISTOR S.M. 100K 1/4W P.6.35
RESISTOR S.M. 100K 1/4W P.6.35
RESISTOR S.M. 100K 1/4W P.6. 35
RESISTOR S.M. 100K 1/4W P.6. 35
RESISTOR S.M. 7K5 1/4W P. 6.35
RESISTOR S.M. 27K 1/4W P.6.35
RESISTOR S.M. 27K 1/4W P. 6.35
RESISTOR S.M. 1K5 1/4W P.6.35















 7 8

RESISTOR S.M. 510 1/4W P. 6.35
RESISTOR S.M. 8K2 1/4W P.6.35
RESISTOR S.M. 270K 1/4W P.7.5
RESISTOR S.M. 82K 1/4W P.6.35
RESISTOR S.M. 91 1/4W P. 6.35
RESISTOR S.M. 180 1/4W P.6.35
RESISTOR S.M. 47K 1/4W P.6.35
RESISTOR S.M. 2K 1/4W P.6. 35
RESISTOR S.M. 68 K 1/4W P. 6.35
RESISTOR S.M. 1M 1/4W P.6.35
RESISTOR S.M. 15K 1/4W P. 6.35
RESISTOR S.M. 6K2 1/4W P.6.35
RESISTOR S.M. 330 1/4W P. 6.35
RESISTOR S.M. 150 1/4W P.6.35
RESISTOR S.M. 3K3 1/4W 0,25\% 25PPM P.6.35*
RESISTOR S.M. 3K3 1/4W 0,25\% 25PPM P.6.35*
RESISTOR S.M. 15K 1/4W 0,25\% 25PPM P.6.35*
RESISTOR S.M. 15K 1/4W 0,25\% 25PPM P.6.35*
SPACER FOR TO-5
SPACER FOR TO-18
TRIMMER 10K CERMET 10T 64Y
TRIMMER 50R CERMET 10T 64Y
TRIMMER 100R CERMET 10T 64Y
TRIMMER 20K CERMET 1T 3362P
UC3844
I.C. LP339N

HCPL-3120
HCPL-3120
I.C. LM336BZ5.0
I.C. LM2902N
I.C. UC3846N

|  | SRFB1K5ALM 48V/70A SMPS REGULATOR POWER SECTION |  |
| :---: | :---: | :---: |
| REF. | DESCRIPTION | Q.ty |
| C1 | CAPACITOR, CERAMIC 2,2NF 1KV P.5.08 | 1 |
| C20 | CAPACITOR, CERAMIC 2,2NF 1KV P.5.08 | 1 |
| C2 | CAPACITOR, CERAMIC 100PF 1KV P.5.08 | 1 |
| C19 | CAPACITOR, CERAMIC 100PF 1KV P.5.08 | 1 |
| C24 | CAPACITOR, CERAMIC 100PF 1KV P.5.08 | 1 |
| C5 | CAPACITOR, POLY. 2,2MF 250V P.22.5 MKT1822 | 1 |
| C16 | CAPACITOR, POLY. 1MF 250V P.22.5 MKT1822 | 1 |
| C21 | CAPACITOR, CER. M.S. $0,22 \mathrm{MF} 100 \mathrm{~V}$ P.5,08 X7R1 | 1 |
| C3 | CAPACITOR, ELECTROLITIC VERT. 1000MF 200V P. $1035 \times 35$ | 1 |
| C4 | CAPACITOR, ELECTROLITIC VERT. 1000MF 200V P. $1035 \times 35$ | 1 |
| C6 | CAPACITOR, ELECTROLITIC VERT. 1000MF 200V P. $1035 \times 35$ | 1 |
| C9 | CAPACITOR, ELECTROLITIC VERT. 1000MF 200V P. $1035 \times 35$ | 1 |
| C17 | CAPACITOR, ELECTROLITIC VERT. 1000MF 200V P. $1035 \times 35$ | 1 |
| C18 | CAPACITOR, ELECTROLITIC VERT. 1000MF 200V P. $1035 \times 35$ | 1 |
| C10 | CAPACITOR, ELECTROLITIC VERT. 1000MF 63V P. $7,518 \times 30$ SXE | 1 |
| C11 | CAPACITOR, ELECTROLITIC VERT. 1000MF 63V P. $7,518 \times 30$ SXE | 1 |
| C12 | CAPACITOR, ELECTROLITIC VERT. 1000MF 63V P. $7,518 \times 30$ SXE | 1 |
| C13 | CAPACITOR, ELECTROLITIC VERT. 1000MF 63V P. $7,518 \times 30$ SXE | 1 |
| C14 | CAPACITOR, ELECTROLITIC VERT. 1000MF 63V P. $7,518 \times 30$ SXE | 1 |
| C15 | CAPACITOR, ELECTROLITIC VERT. 1000MF 63V P.7,5 18x30 SXE | 1 |
| C22 | CAPACITOR, ELECTROLITIC VERT. 220MF 25 V P. 5.08 | 1 |
| C27 | CAPACITOR, ELECTROLITIC VERT. 220MF 25 V P. 5,08 | 1 |
| C23 | CAPACITOR, ELECTROLITIC VERT. 47MF 63V P.3,5 LXF | 1 |
| C25 | CAPACITOR, ELECTROLITIC AX. 10MF 40/63V P.17,5 | 1 |
| C26 | CAPACITOR, ELECTROLITIC AX. 10MF 40/63V P.17,5 | 1 |
| C7 | OMITTED | 1 |
| C8 | OMITTED | 1 |
| CR1 | DIODE ZENER BZX85C18 | 1 |
| CR2 | DIODE ZENER BZX85C18 | 1 |
| CR15 | DIODE ZENER BZX85C18 | 1 |
| CR16 | DIODE ZENER BZX85C18 | 1 |
| CR3 | DIODE MUR115/BYV27-200 | 1 |
| CR5 | DIODE MUR115/BYV27-200 | 1 |
| CR6 | DIODE MUR115/BYV27-200 | 1 |
| CR13 | DIODE MUR115/BYV27-200 | 1 |
| CR14 | DIODE MUR115/BYV27-200 | 5 |
| CR4 | DIODE ZENER BZX55C20 | 1 |
| CR7 | DIODE BYV10-40/1N5819 | 1 |
| CR8 | DIODE BYV10-40/1N5819 | 1 |
| CR9 | DIODE BYV10-40/1N5819 | 1 |
| CR10 | DIODE BYV10-40/1N5819 | 1 |
| CR11 | DIODE BYV10-40/1N5819 | 1 |
| CR12 | DIODE BYV10-40/1N5819 | 6 |
| CR17 | DIODE BYV27-200 | 1 |
| CR18 | DIODE BYV27-200 | 1 |
| CR19 | DIODE BYV27-200 | 1 |
| CR20 | DIODE BYV255-V200 | 1 |
| DT1 | HEATSINK | 1 |
| E1 | TEFZER WIRE D2,5mm | 13 cm |
| E2 | SHEATHED WIRE JUMPER | 1 |
| E3 | OUTPUT BAR | 1 |
| E4 | OUTPUT BAR | 1 |
| E5 | BUS BAR PART. C W. 0089 | 1 |


| E6 | \|BUS BAR PART. D W. 0089 | 1 |
| :---: | :---: | :---: |
| E7 | BUS BAR PART. E W. 0089 | 1 |
| E8 | BUS BAR PART. F W. 0089 | 1 |
| E9 | BUS BAR PART. G W. 0089 | 2 |
| E10 | BUS BAR PART. H W. 0089 | 1 |
| F1 | FUSE, SUPER FAST L350-80/80LET | 1 |
| FL1 | FILTER INDUCTOR | 1 |
| L1 | INDUCTOR 22uH D46 | 1 |
| L2 | INDUCTOR 22uH D46 | 1 |
| CS1 | PRINTED CIRCUIT | 1 |
| P1 | STRAIGHT CONNECTOR 16P, 2.54 L.P. | 1 |
| P2 | STRAIGHT CONNECTOR 9P, 2.54 L.P. | 1 |
| PTC1 | PTH9M04-BD/471TS2F333 | 1 |
| Q1 | MOSFET IRFP250 | 1 |
| Q2 | MOSFET IRFP250 | 1 |
| Q3 | MOSFET IRFP250 | 1 |
| Q4 | MOSFET IRFP250 | 1 |
| Q5 | MOSFET IRFP250 | 1 |
| Q6 | MOSFET IRFP250 | 1 |
| Q7 | MOSFET IRF720 | 1 |
| R1 | RESISTOR MET. OXIDE 22 3W 5\% p. 20 | 1 |
| R2 | RESISTOR MET. OXIDE 22 3W 5\% p. 20 | 1 |
| R4 | RESISTOR MET. OXIDE 10 3W 5\% p. 20 | 1 |
| R24 | RESISTOR MET. OXIDE 10 3W 5\% p. 20 | 1 |
| R5 | RESISTOR S.M. 1K 1/2W | 1 |
| R6 | RESISTOR MET. OXIDE 4,7 2W 5\% p. 15 | 1 |
| R7 | RESISTOR S.M. 4K7 1/2W | 1 |
| R26 | RESISTOR S.M. 4K7 1/2W | 1 |
| R27 | RESISTOR S.M. 4K7 1/2W | 1 |
| R28 | RESISTOR S.M. 4K7 1/2W | 1 |
| R8 | RESISTOR S.M. 4,7 1/2W | 1 |
| R9 | RESISTOR S.M. 4,7 1/2W | 1 |
| R10 | RESISTOR S.M. 4,7 1/2W | 1 |
| R11 | RESISTOR S.M. 4,7 1/2W | 1 |
| R12 | RESISTOR S.M. 4,7 1/2W | 1 |
| R13 | RESISTOR S.M. 4,7 1/2W | 1 |
| R 14 | RESISTOR MET. OXIDE 47K 2W 5\% P.17,5 | 1 |
| R 15 | RESISTOR S.M. 47 1/2W | 1 |
| R16 | RESISTOR S.M. 151/2W | 1 |
| R17 | RESISTOR S.M. 151/2W | 1 |
| R18 | RESISTOR S.M. 151/2W | 1 |
| R19 | RESISTOR S.M. 151/2W | 1 |
| R20 | RESISTOR S.M. 151/2W | 1 |
| R21 | RESISTOR S.M. 151/2W | 1 |
| R22 | RESISTOR S.M. 2K2 1/2W | 1 |
| R23 | RESISTOR S.M. 2K2 1/2W | 1 |
| R 25 | RESISTOR MET. OXIDE 6,8 2W 2\% P. 20 | 1 |
| R 29 | RESISTOR MET. OXIDE 2K2 3W 5\% P. 22.5 | 1 |
| R30 | RESISTOR MET. OXIDE 4K7 3W 5\% P. 22.5 | 1 |
| R31 | RESISTOR MET. OXIDE 4K7 3W 5\% P. 22.5 | 1 |
| R32 | RESISTOR MET. OXIDE 4K7 3W 5\% P. 22.5 | 1 |
| ,R33 | RESISTOR MET. OXIDE 4K7 3W 5\% P. 22.5 | 1 |
| R 3 | OMITTED | 1 |
| SCR1 | SCR S2065K | 1 |
| SH1 | LOW OHM WIRE RESISTOR D3mm L=23 | 1 |
| SH2 | LOW OHM WIRE RESISTOR D3mm L=23 | 1 |
| SH3 | LOW OHM WIRE RESISTOR D3mm L=23 | 1 |

# SRFB1K0PB2 - 2 PORT RF OUTPUT COMBINER \& LPF 

REF.

C2
C1
C3
C8
C5
C4
C6
C7
C9
D1
D2
L1
L2
R5
R6
R3
R7
R14
R4
R12
R13
R10
R11

AUXILIARY PRINTED CIRCUIT
AUXILIARY PRINTED CIRCUIT
CAPACITOR CHIP CERAM. 1206 33pF 5\% 100V NPO CAPACITOR CHIP CERAM. 1206 33pF 5\% 100V NPO CAPACITOR CHIP CERAM. 1206 47pF 5\% 100V NPO CAPACITOR CHIP CERAM. 1206 220pF 5\% 100V NP0 CAPACITOR CHIP CERAM. 1206 220pF 5\% 100V NP0 CAPACITOR CHIP CERAM. 1206 220pF 5\% 100V NP0 CAPACITOR CHIP CERAM. 1206 220pF 5\% 100V NP0
DIODE BAT54S SOT23 DUAL SCHOTTKY .2A/30

DIODE BATJ4S SOT23 DUAL SCHOTTKY .2A/30
DIODE BAT54S SOT23 DUAL SCHOTTKY .2A/30
RF LINE
INDUCTOR TOROIDAL FERRITE F2 D16x8sp10
RESISTOR CHIP 120618 OHM 1/4W 1\%
RESISTOR CHIP 1206120 OHM 1/4W 1\%
RESISTOR CHIP 1206150 OHM 1/4W 1\%
RESISTOR CHIP 1206150 OHM 1/4W 1\%
RESISTOR CHIP 1206270 OHM 1/4W 1\%
RESISTOR CHIP 1206330 OHM 1/4W 1\%
RESISTOR CHIP 1206 1.OK OHM 1/4W 1\%
RESISTOR CHIP 1206 1.0K OHM 1/4W 1\%
RESISTOR FLANGED 250W 50 OHM
RESISTOR FLANGED 250W 50 OHM

|  | SRFB500W - 500W AMPLIFIER MODULE |  |  |
| :---: | :---: | :---: | :---: |
| REF. | DESCRIPTION | Q.ty | MANUFACTURER |
| C1 | CAPACITOR SMD 33pF 100V COG | 1 |  |
| C2 | CAPACITOR, SMD 10pF 100 V COG | 1 |  |
| C3 | CAPACITOR, SMD 22pF 100 V COG | 1 |  |
| C4 | CAPACITOR, SMD 22 pF 100 V COG | 1 |  |
| C5 | CAPACITOR, SMD 100pF 200 V COG | 1 |  |
| C6 | CAPACITOR, SMD 100pF 200 V COG | 1 |  |
| C7 | CAPACITOR, SMD 100pF 200 V COG | 1 |  |
| C8 | CAPACITOR, SMD 100pF 200V COG | 1 |  |
| C9 | CAPACITOR, CER NP0 47pF 100 V | 1 |  |
| C10 | CAPACITOR, CER NP0 47pF 100V | 1 |  |
| C11 | CAPACITOR, SMD 1nF 100V COG | 1 |  |
| C12 | CAPACITOR, SMD 1nF 100V COG | 1 |  |
| C13 | CAPACITOR, SMD 1nF 100V COG | 1 |  |
| C14 | CAPACITOR, SMD 1nF 100V COG | 1 |  |
| C16 | CAPACITOR, CERAMIC 470pF 100 V | 1 |  |
| C16 | CAPACITOR, CERAMIC 470pF 100 V | 1 |  |
| C17 | CAPACITOR, CERAMIC 470pF 100 V | 1 |  |
| C18 | CAPACITOR, CERAMIC 470pF 100 V | 1 |  |



| TR3 | VHF OUTPUT TRANSFORMER | 1 | SIEL |
| :--- | :--- | :--- | :--- |
| TR4 | VHF OUTPUT TRANSFORMER | 1 | 1 |
| Z 1 | BRASS M4 TC STUD | 1 |  |
| Z 1 | 400W RF AMPLIFIER PCB | 1 |  |

